




**Statens vegvesen**  
Norwegian Public Roads  
Administration



# Improving bearing capacity assessment by applying temperature correction models

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# Bearing capacity

*'The maximum axle load a road can handle over a period of time (the design period), while the condition of the road with normal maintenance does not fall below a defined acceptable limit (N200, Statens vegvesen).'*

$$B = 11 \cdot \left( \frac{E_{\text{dim}}}{200} \right)^{0.6} \cdot \left( \frac{50}{AADT_T} \right)^{0.072}$$

B : bearing capacity (tons)

$E_{\text{dim}}$  : design surface modulus (MPa)

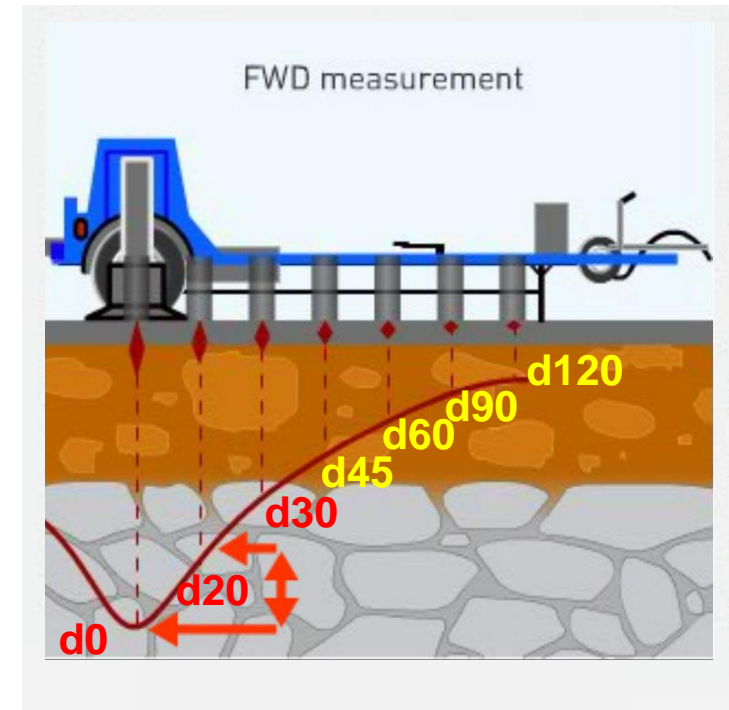
$AADT_T$  : annual average daily traffic for heavy vehicles

$$E_{\text{dim}} = 110 \cdot \frac{p}{(\delta_0 \cdot (\delta_0 - \delta_{200}))^{0.5}}$$

p : contact pressure (MPa)

$\delta_0$  : deflection at the load center (mm)

$\delta_{200}$  : deflection 200 mm from the load center (mm)



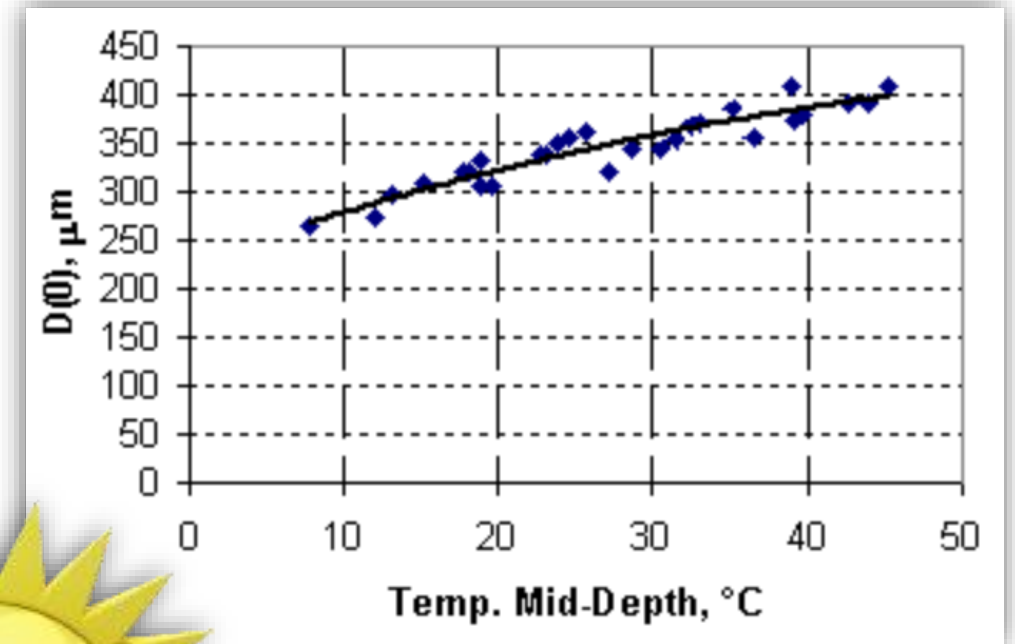
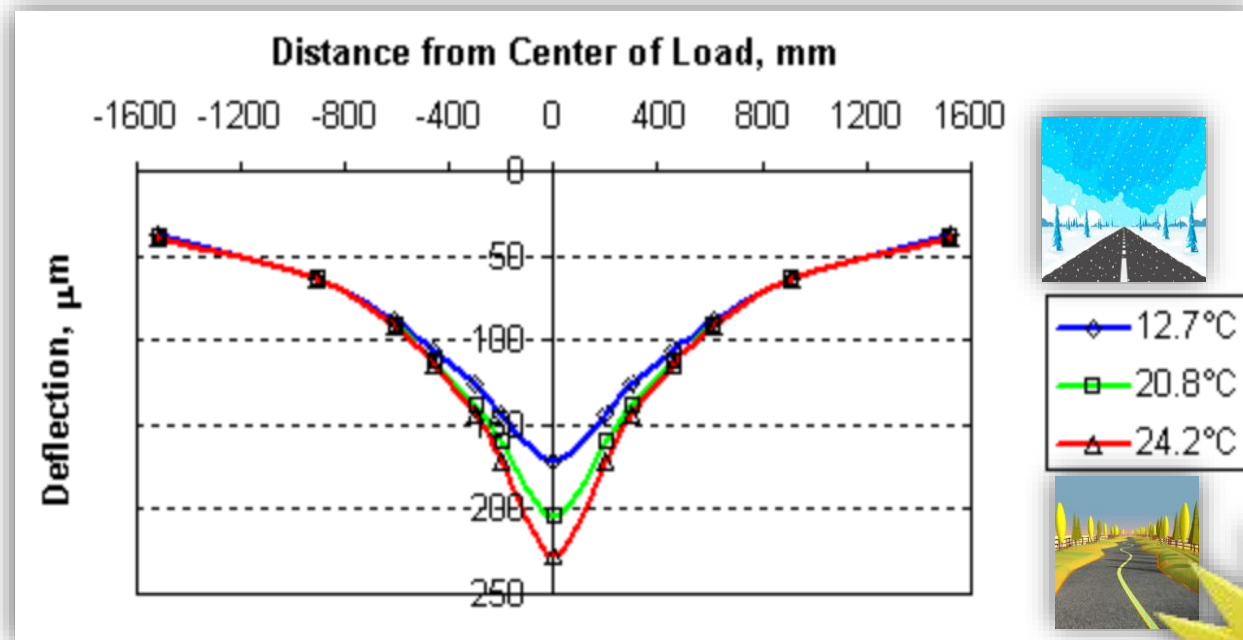
Surface Curvature Index (SCI) =  $d_0 - d_{20}$

Base Curvature Index (BCI) =  $d_{90} - d_{120}$

# Why temperature?

## **FHWA** LTPP Guide to Asphalt Temperature Prediction and Correction (FHWA-RD-98-085)

With the trend toward mechanistic-empirical design methods, methods to adjust the pavement response for temperature are needed (1993).

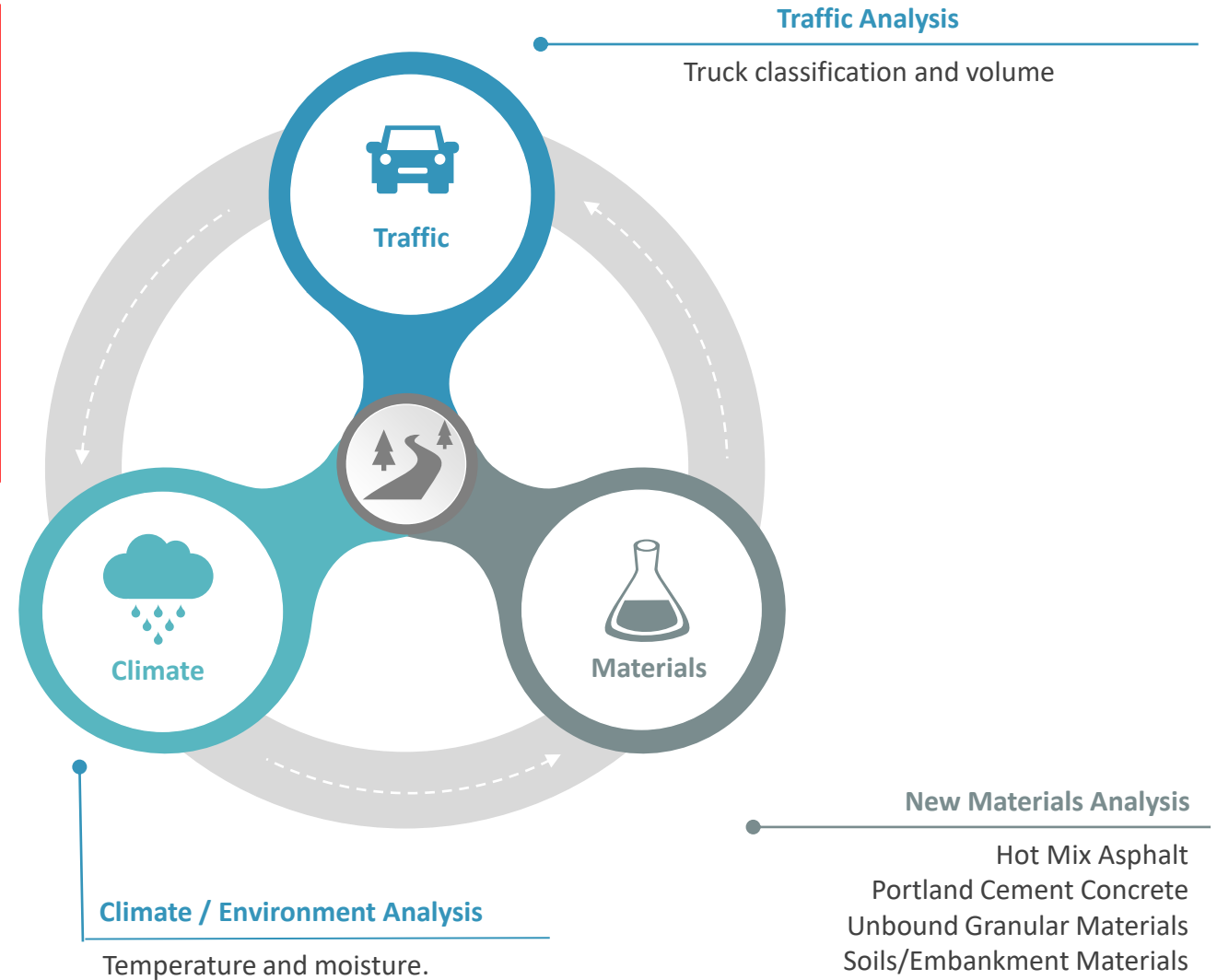
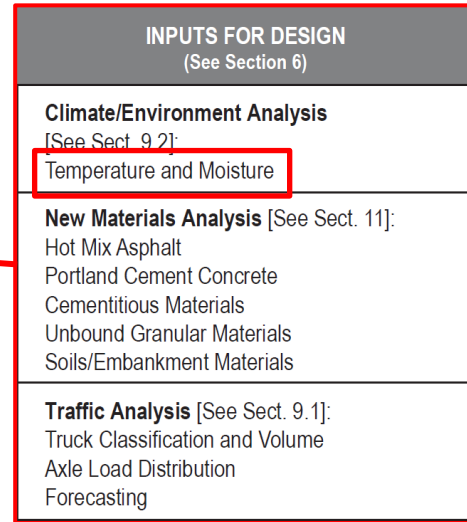
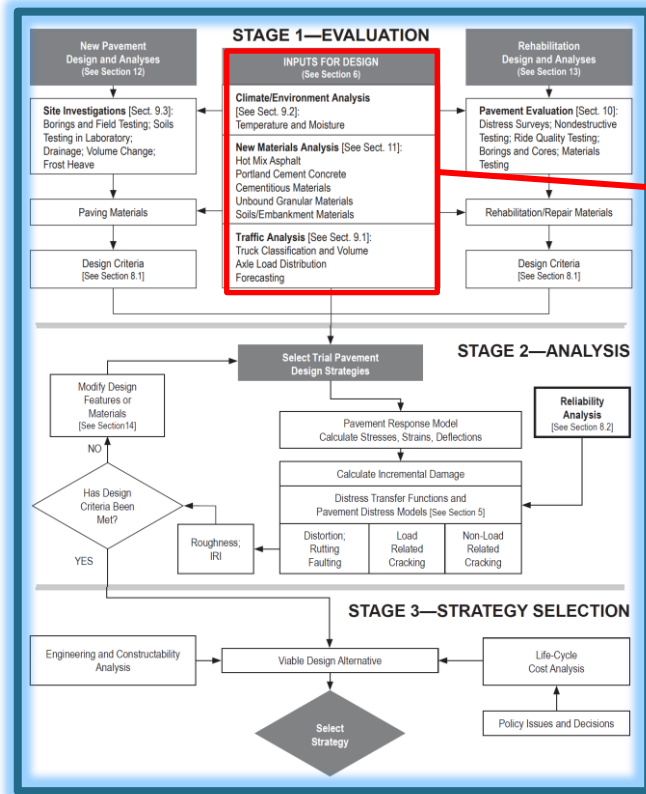


*Same section, over the course of a few hours*

*Same section, over the year*



# Mechanistic Empirical (M-E) design



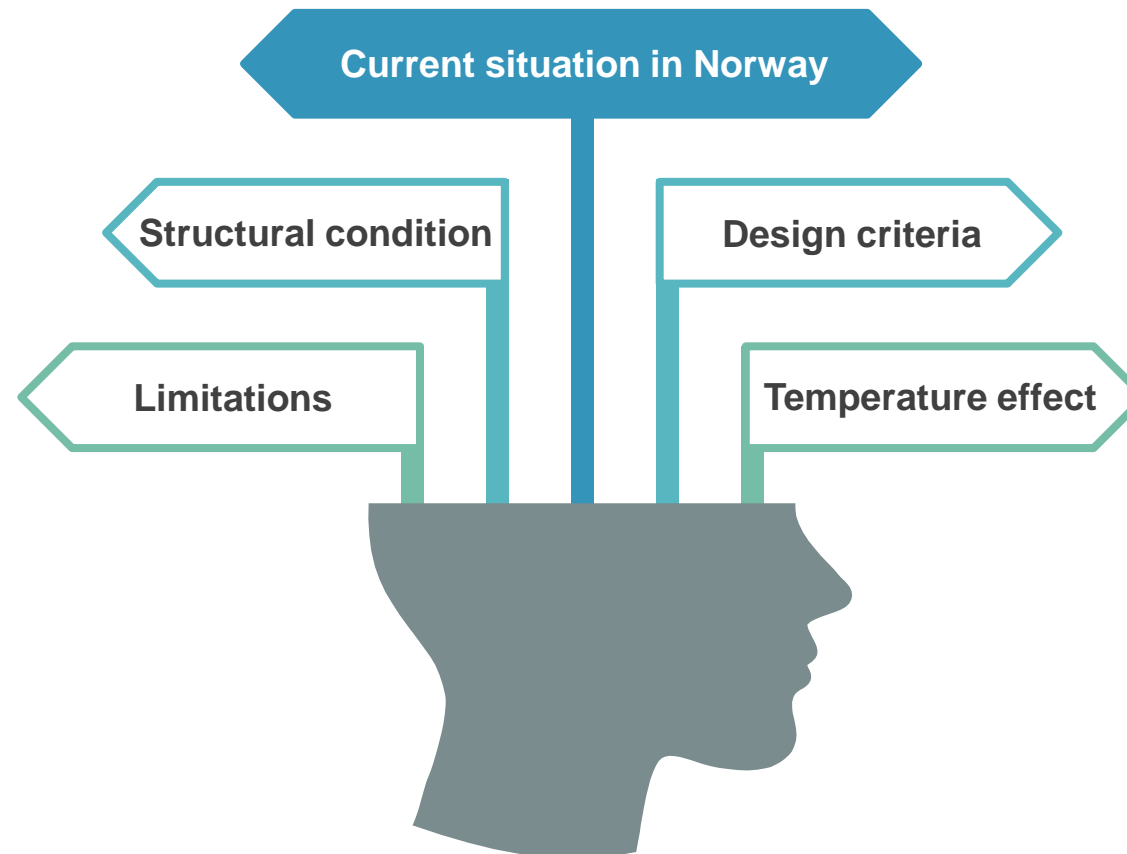
# Project research questions

## How do measure and present structural condition of roads?

By performing Falling Weight Deflectometer (FWD) and presenting FWD parameters as well as using the equation to obtain the value as bearing capacity

## Why we are limited to old-fashioned equations

- Old-fashioned view to road design and technology
- Lack of enough information about the existing roads
- Limited resource and relevant research



## Do we use M-E design method?

There will be a shift in the future towards M-E design method: ERAPave PP software (VegDim)

## Do we consider the effect of temperature in bearing capacity calculations

No! However, a simple empirical formula developed 40 years ago is used and gives relatively acceptable results.

$$B_{korr} = \frac{B}{1,3 - 0,015 \cdot T}$$

$B_{korr}$ : korrigert bæreevne [tonn]  
 $B$ : opprinnelig bæreevne [tonn]  
 $T$ : temperatur midt i dekket [°C]



# The Project team



**Per Otto Aursand**



**Kim Rune Grannes**



**Sara Anastasio**



**Leif Bakløkk**



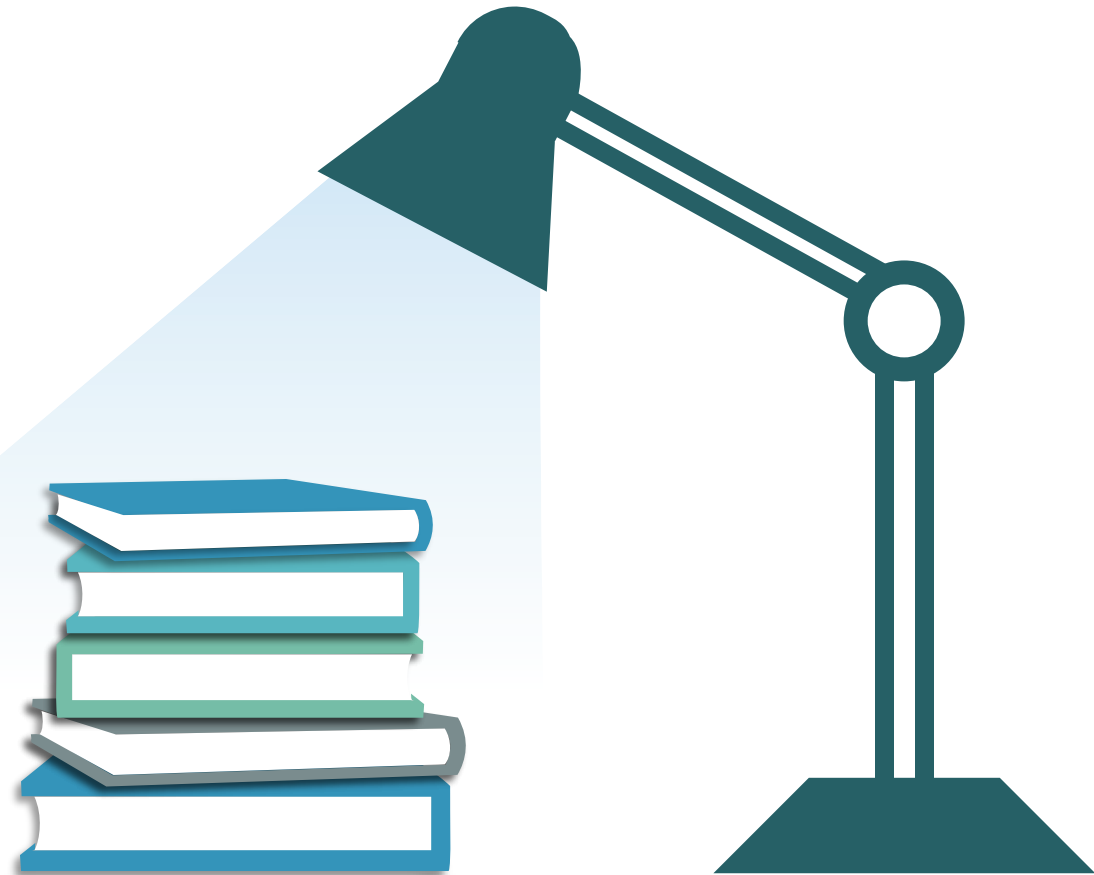
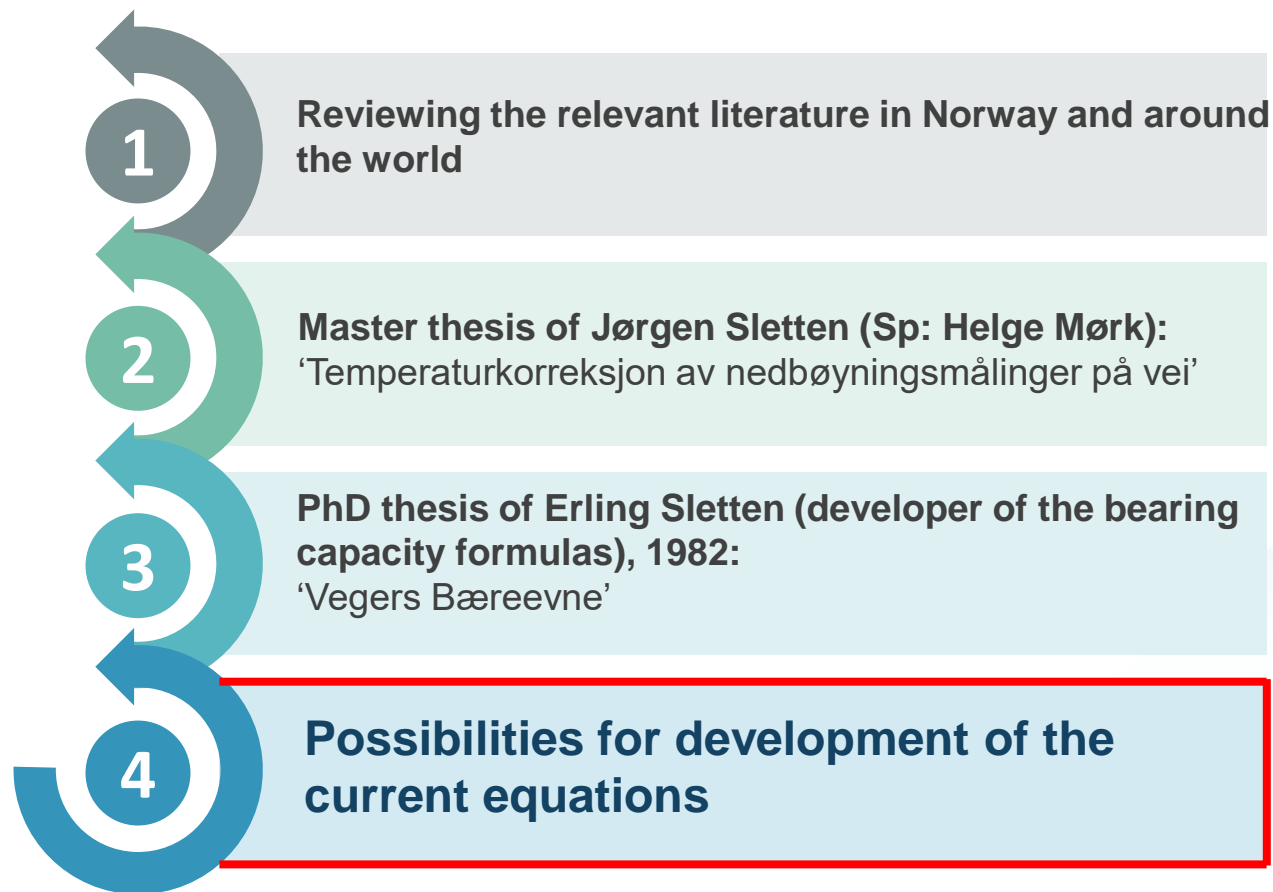
**Trond Østen**



**Ali Mirhosseini**



# Review of the literature



# Measurements with **FWD**, **Raptor**, and **TSD**

On four same stretches

## Objectives:

- Validation and comparison of data, particularly with FWD
- Finding possible correlations based on the measurements
- Further analysis of additional data from Raptor



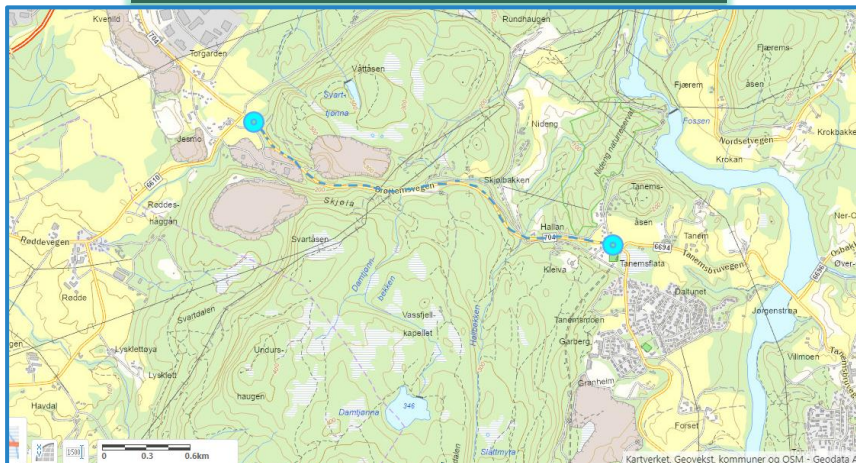


# Test stretches



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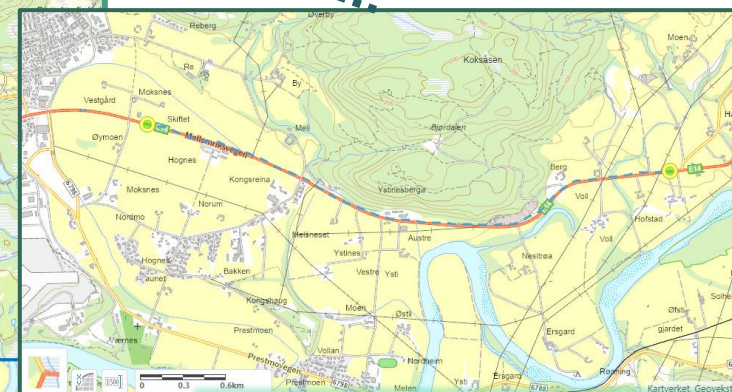
Fv 704 S2 D1 m0 to 2850



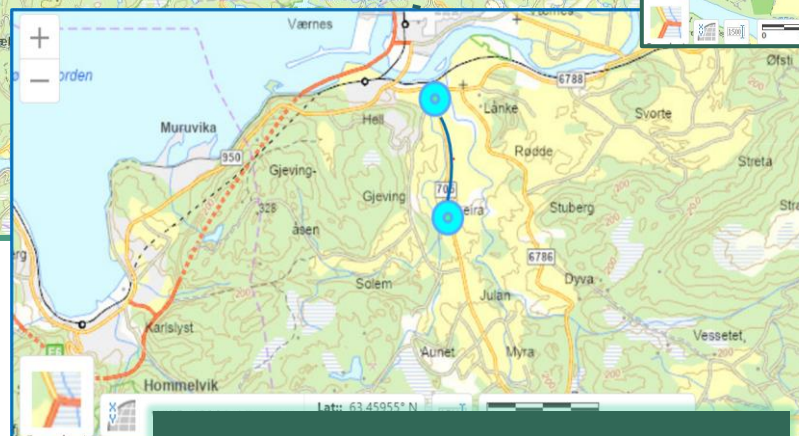
E14 S1 D1 m1700 to 2200



E14 S2 D1 m0 to 4000

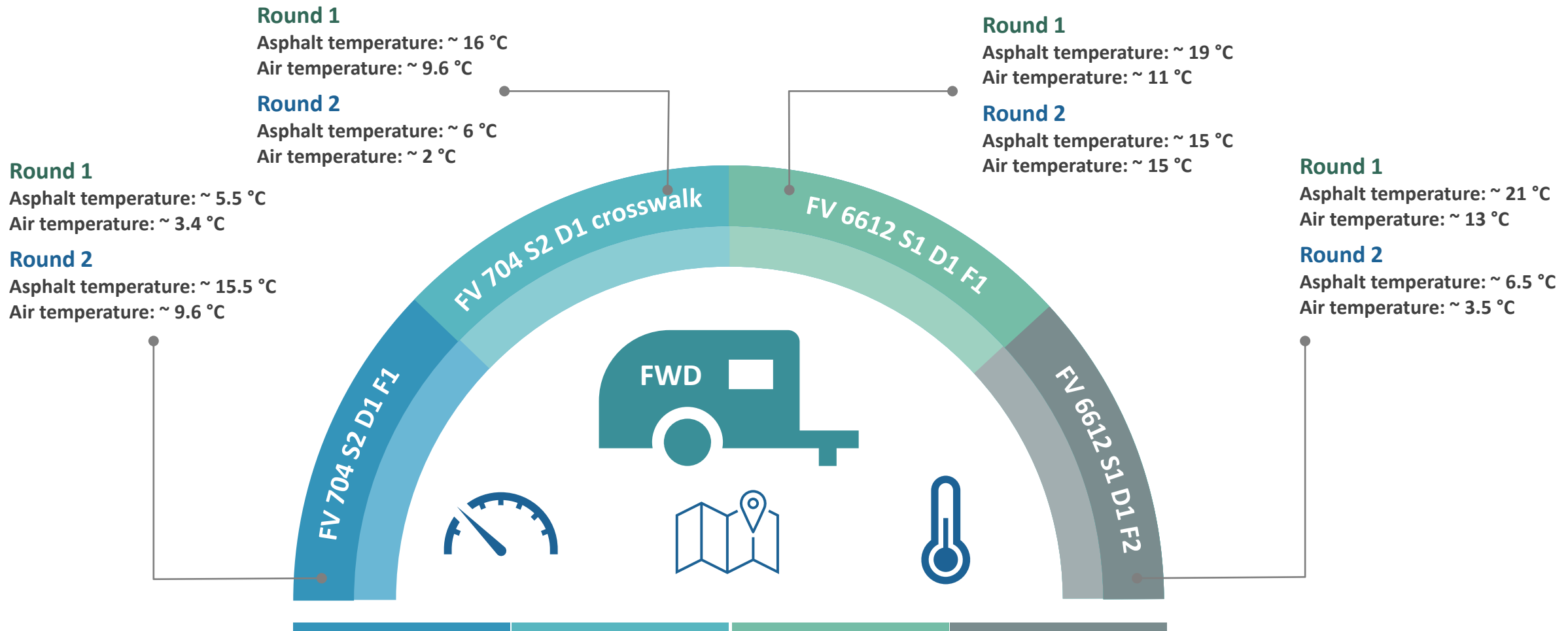


Fv 705 S1 D1 m540 to 3190



# Measurements with FWD

Several times on the same stretches, different temperatures



# Present data

Fv 6612 S1 D1 F1



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DTemp[°C]	LTemp[°C]
19.5	11.3
19.6	11.3
19.3	11.2
18.9	11.1
18.3	11.0
18.6	10.9
18.4	11.0
18.4	11.1
19.4	11.1
20.0	11.2
20.7	11.3
20.1	11.5
19.5	11.6
19.2	11.6
19.5	11.6
19.0	11.6

DTemp[°C]	LTemp[°C]
5.5	2.9
5.6	3.0
5.7	3.0
5.6	3.0
5.4	3.0
5.5	3.0
5.4	3.0
5.5	3.0
5.7	3.0
5.8	3.1
6.0	3.2
6.0	3.3
6.3	3.3
6.3	3.4
6.4	3.4
6.4	3.4

## Round 1

Asphalt temperature: ~ 19 °C

Air temperature: ~ 11 °C

		SCI				BCI								
Bæreevne	D90	D0-D20	D0/(D0-D20)	F-diff	D90-D120	Styrke bærelag	Styrke undergrunn/ forsterkningslag	Sannsynlig undergrunn	Største svakhet i	Undergrunnens E-mod	Tøyning underkant asfalt			
18.7	102.2	52.9	5.5	0.0	27.0	Meget God	God	Sand/grus	F/U	149.1	136.6			
19.2	103.2	51.4	5.4	0.0	24.5	Meget God	God	Sand/grus	F/U	163.4	136.9			
20.0	107.0	49.9	5.1	0.0	21.6	Meget God	God	Sand/grus	F/U	193.8	134.8			
20.6	100.8	42.4	6.2	0.0	26.3	Meget God	God	Sand/grus	F/U	166.8	124.6			
19.2	99.9	50.0	5.8	0.0	27.6	Meget God	God	Sand/grus	F/U	155.0	133.6			
20.4	100.6	41.0	7.1	0.0	32.1	Meget God	God	Sand/grus	F/U	143.1	124.0			
21.0	71.8	45.7	5.1	0.0	17.1	Meget God	Meget god	Sand/grus	F/U	209.2	125.6			
21.3	61.8	43.3	5.4	0.0	21.0	Meget God	God	Sand/grus	F/U	211.3	123.2			
20.8	111.7	38.1	7.6	0.0	32.9	Meget God	God	Sand/grus	F/U	135.9	116.2			
18.9	110.3	48.3	6.4	0.0	31.4	Meget God	God	Sand/grus	F/U	140.4	135.5			
21.0	110.0	38.9	7.0	0.0	28.4	Meget God	God	Sand/grus	F/U	140.2	113.2			
19.8	75.5	50.9	5.0	0.0	21.1	Meget God	God	Sand/grus	B/F	197.0	135.9			
17.2	94.3	66.6	4.7	0.0	26.4	Meget God	God	Sand/grus	B/F	161.3	156.8			
16.1	100.2	71.6	5.1	0.0	23.0	Meget God	God	Sand/grus	F/U	153.4	180.9			
15.2	126.2	71.3	6.2	0.0	36.5	Meget God	God	Sand/grus	F/U	124.6	198.4			
17.4	105.3	56.3	6.2	0.0	30.5	Meget God	God	Sand/grus	F/U	146.3	165.9			

## Round 2

Asphalt temperature: ~ 15 °C

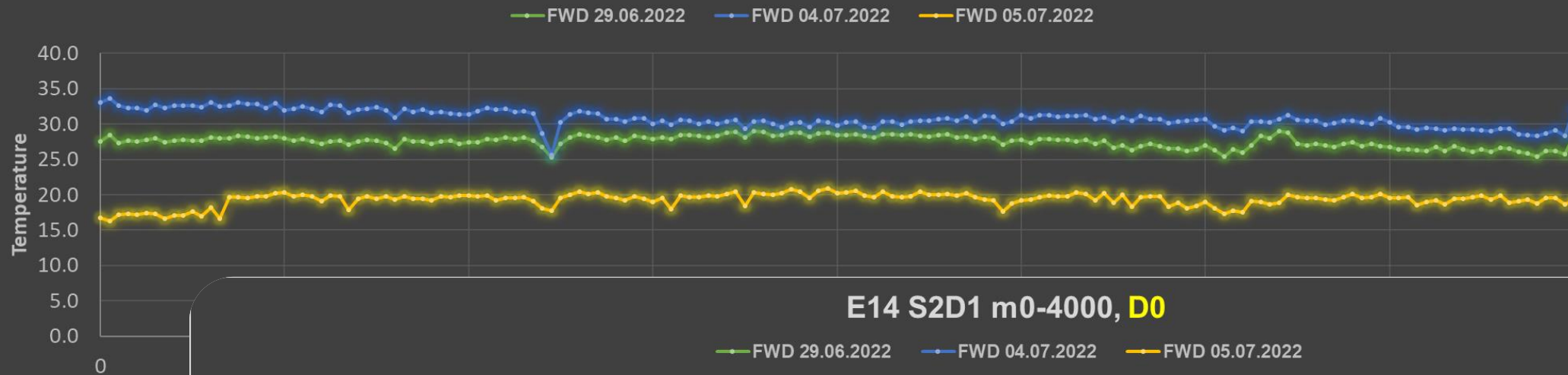
Air temperature: ~ 15 °C

		SCI				BCI							
Bæreevne	D90	D0-D20	D0/(D0-D20)	F-diff	D90-D120	Styrke bærelag	Styrke undergrunn/ forsterkningslag	Sannsynlig undergrunn	Største svakhet i	Undergrunnens E-mod	Tøyning underkant asfalt		
24.3	104.9	32.3	7.8	0.0	26.4	Meget God	God	Sand/grus	F/U	146.6	107.0		
24.5	95.2	32.2	7.7	0.0	21.9	Meget God	God	Sand/grus	F/U	159.9	110.2		
22.9	107.6	40.6	6.1	0.0	26.5	Meget God	God	Sand/grus	F/U	172.7	111.2		
25.7	90.5	30.2	7.5	0.0	23.5	Meget God	God	Sand/grus	F/U	167.5	98.5		
24.7	101.7	31.2	8.0	0.0	26.6	Meget God	God	Sand/grus	F/U	150.8	103.5		
25.4	101.9	28.4	8.8	0.0	26.2	Meget God	God	Sand/grus	F/U	149.2	100.1		
27.5	71.4	28.4	6.8	0.0	19.9	Meget God	Meget god	Sand/grus	F/U	210.3	96.8		
26.5	71.6	30.1	6.8	0.0	21.5	Meget God	God	Sand/grus	F/U	204.3	101.2		
26.6	101.3	25.2	9.5	0.0	29.7	Meget God	God	Sand/grus	F/U	141.2	89.8		
24.3	111.4	30.6	8.8	0.0	36.8	Meget God	God	Sand/grus	F/U	134.8	104.3		
27.5	105.0	23.9	9.5	0.0	26.7	Meget God	God	Sand/grus	F/U	146.3	88.2		
26.5	74.7	30.6	6.6	0.0	16.5	Meget God	Meget god	Sand/grus	F/U	199.1	99.4		
21.6	103.4	44.1	6.3	0.0	26.4	Meget God	God	Sand/grus	F/U	163.1	131.8		
19.5	102.0	51.6	6.5	0.0	29.1	Meget God	God	Sand/grus	F/U	150.9	157.0		
17.2	130.7	63.0	6.5	0.0	33.7	Meget God	God	Sand/grus	F/U	120.5	177.4		
19.8	104.2	49.7	6.5	0.0	28.3	Meget God	God	Sand/grus	F/U	147.5	150.2		

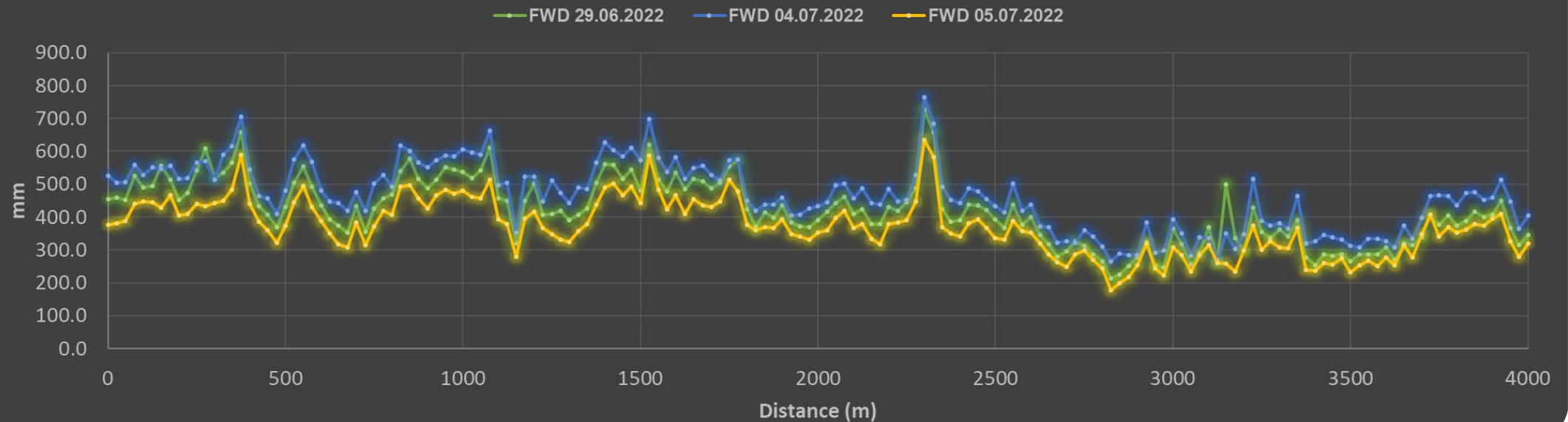


# Present data

E14 S2D1 m0-4000  
Asphalt surface temperature



E14 S2D1 m0-4000, D0





## Possibilities for development

Use of temperature prediction models (e.g., BELLS), correlation analysis, calibrating based on Norwegian data

Calibrating the formulas that we currently have based on available and more measurements

Carrying out core drilling to determine pavement information (e.g., layers thickness) to include E-modulus in estimation and consequently performing backcalculation analysis

Use of backcalculation, determining deflection factors, calculating E-modulus, and calibrating

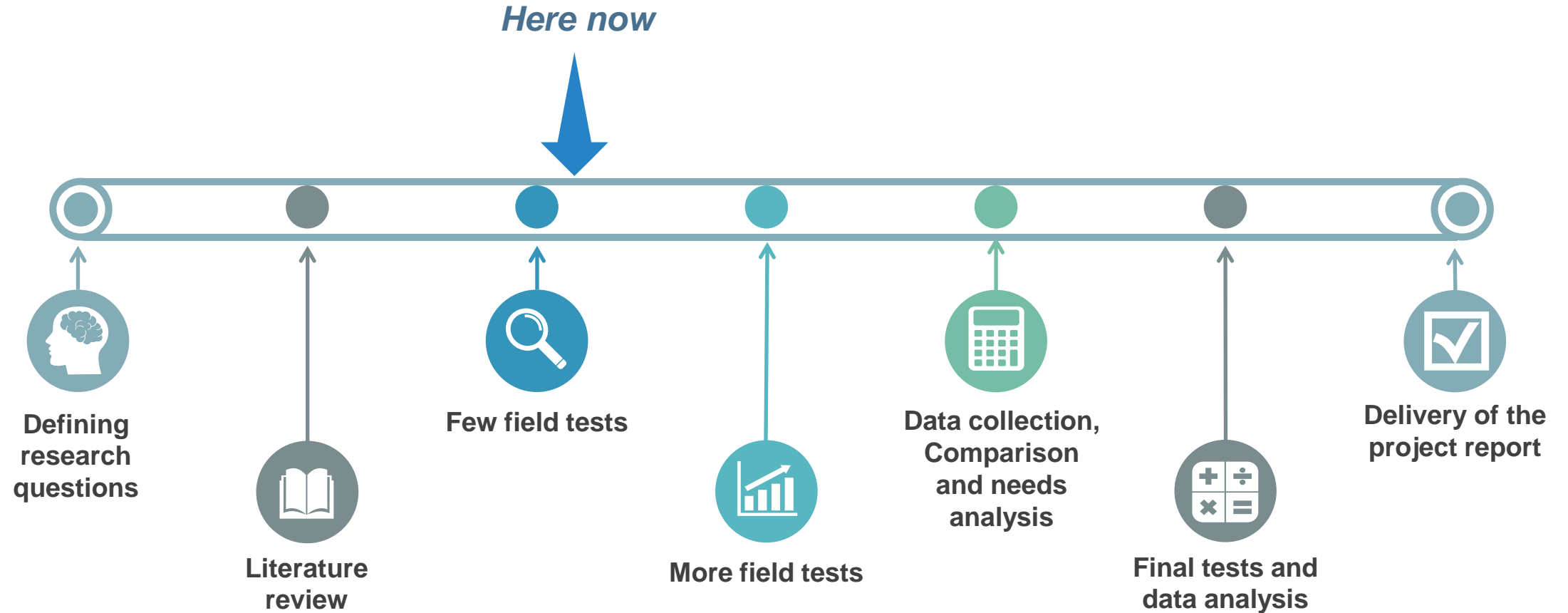
?

**Practical /  
national level**

**Project level**



# Project status



# Limitations / risk factors



- 1 Lack of enough information on the road's construction
- 2 Challenges with performing FWD on E6 (main roads)
- 3 Carrying out FWD measurements is costly
- 4 Limited test area cannot be a good representative of whole Norway
- 5 What do you think ... ?



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**Thank you!**