

Frost in open-graded materials

Karlis Rieksts
PhD



Introduction and background



Large scale experimental setup and results



Field test site description and temperature distribution analysis

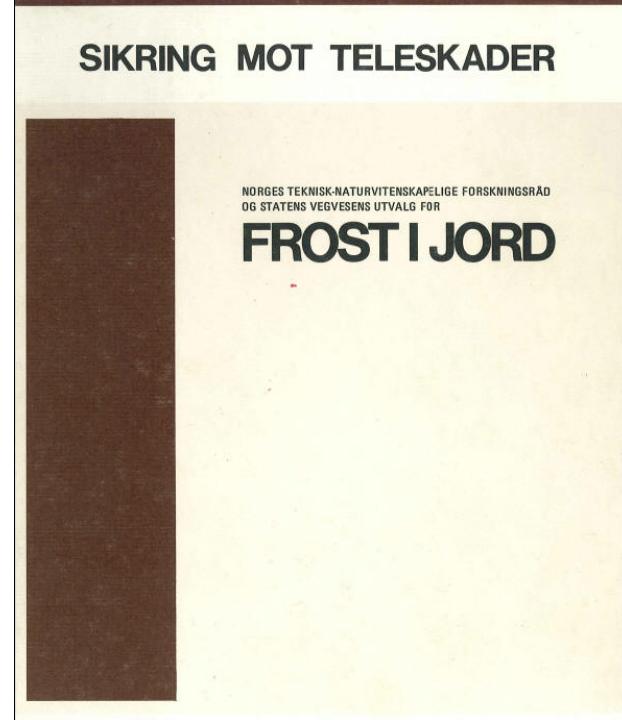


Numerical model of field test site



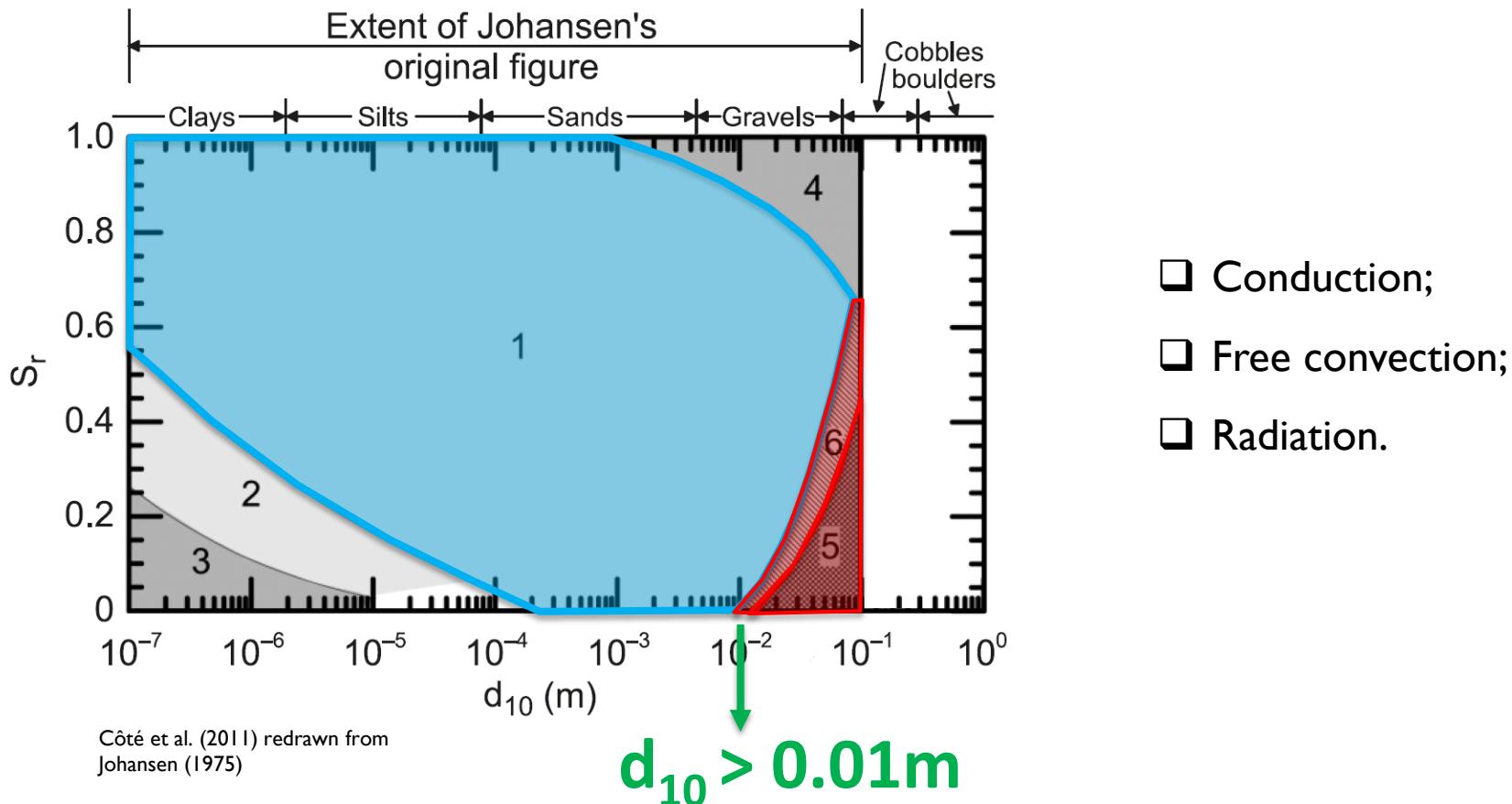
Conclusions

- The use of crushed rock materials;
- Frost heave on newly built roads/railways;
- Requirements for frost protection layers;
- Other coarse construction materials.



Open-graded materials in road construction

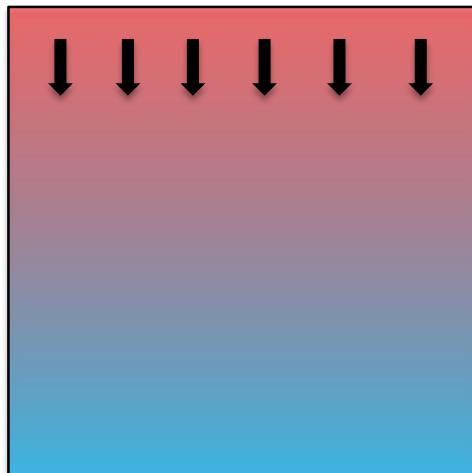




Theory on natural air convection

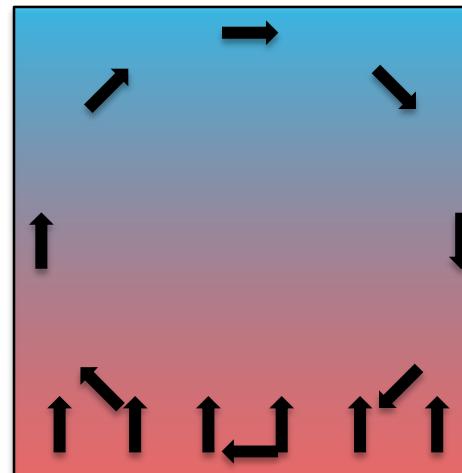
Downward heat flow

$$\mathbf{q} \downarrow$$



Upward heat flow

$$\mathbf{q} \uparrow$$



- conduction
 - radiation
- ➡ effective thermal conductivity

- conduction
 - radiation
- convection

Theory on natural air convection

Nu

Nusselt number

$$\text{Nu} = \frac{q\uparrow}{q\downarrow}$$

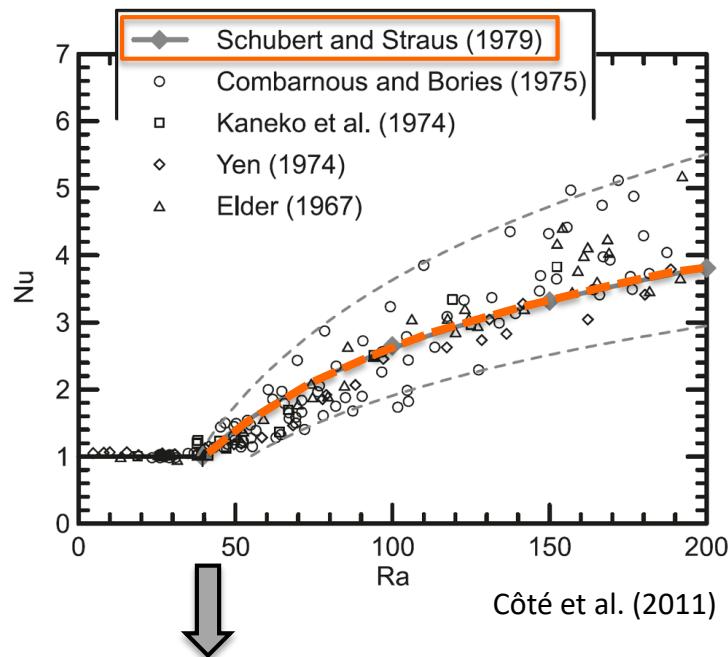
 $q\uparrow$ - upward heat flow $q\downarrow$ - downward heat flow**Ra**

Rayleigh number

$$\text{Ra} = \frac{g \beta C K H^2 \nabla T}{\nu k_e}$$

 g gravitational acceleration β thermal expansion C heat capacity ν kinematic viscosity K intrinsic permeability H height ∇T temperature gradient k_e effective thermal conductivity

Theory on natural air convection



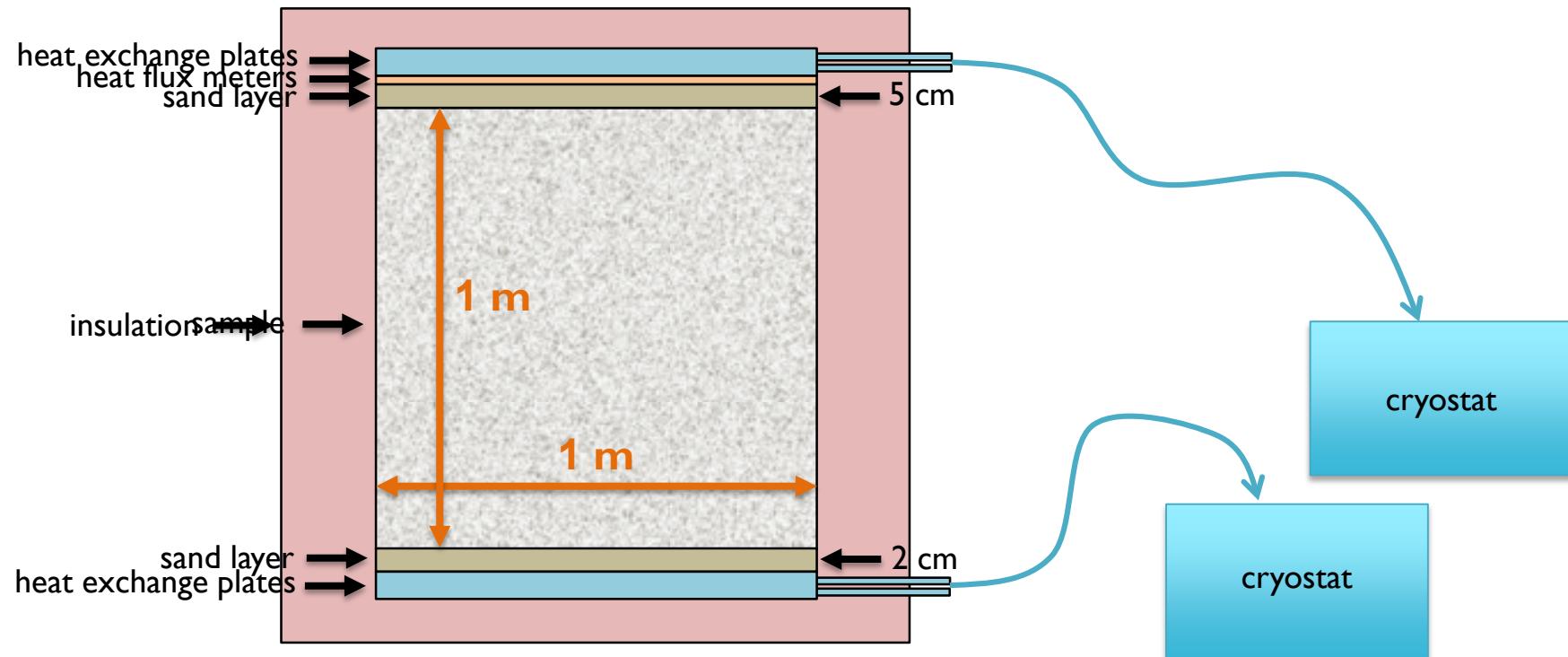
$$\text{Nu} = 1.735 \ln(\text{Ra}) - 5.38$$

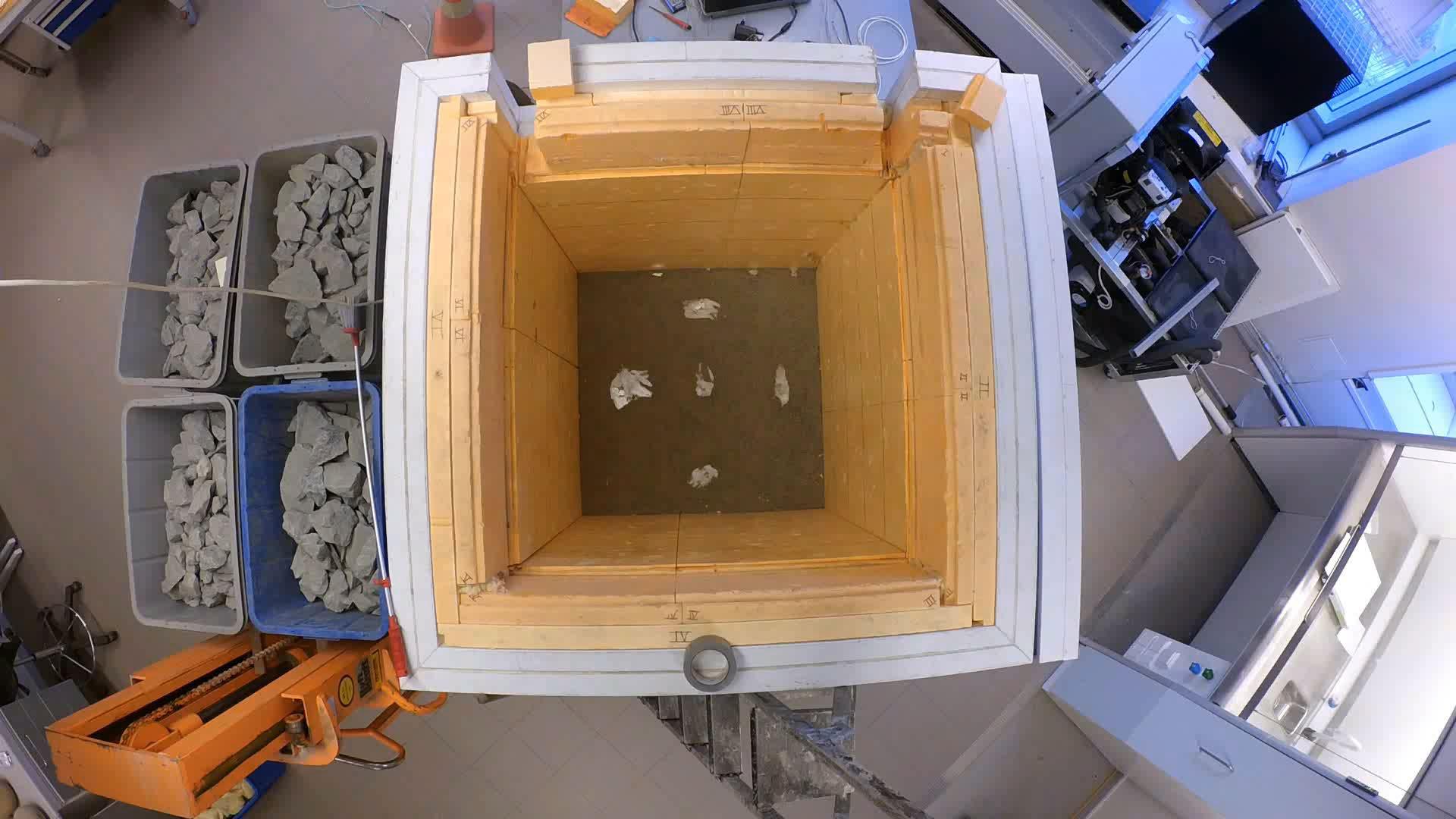


$$\frac{q \uparrow}{q \downarrow} = 1.735 \ln \left(\frac{g\beta CKH^2 \nabla T}{\nu k_e} \right) - 5.38$$

Critical Rayleigh number:

$$\text{Ra}_c = \sim 40$$

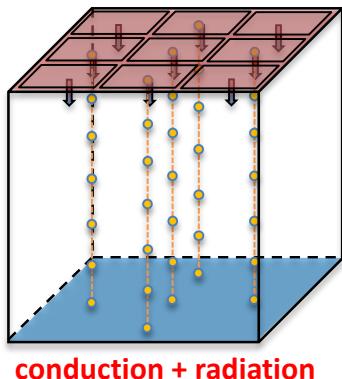




Experimental procedure

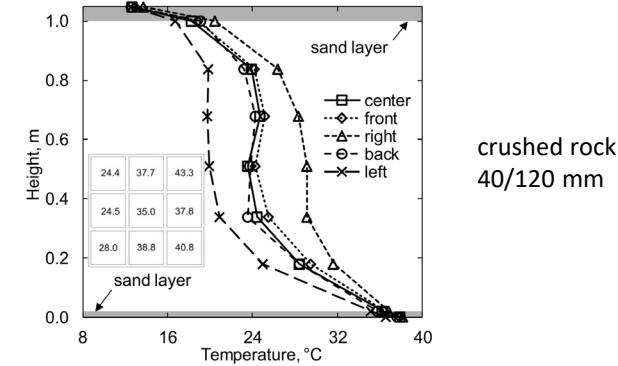
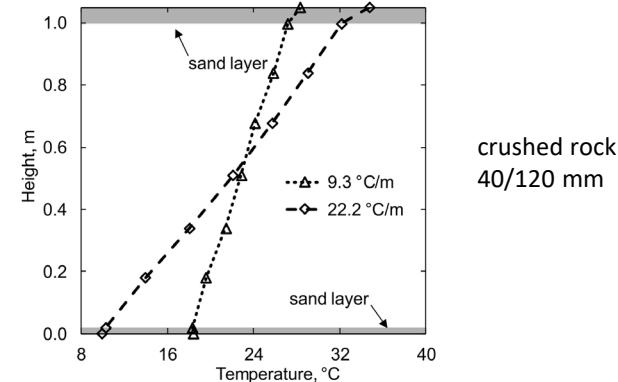
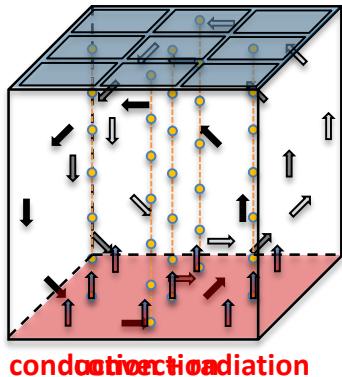
Downward heat flow:

$$\mathbf{q} = -\nabla T$$

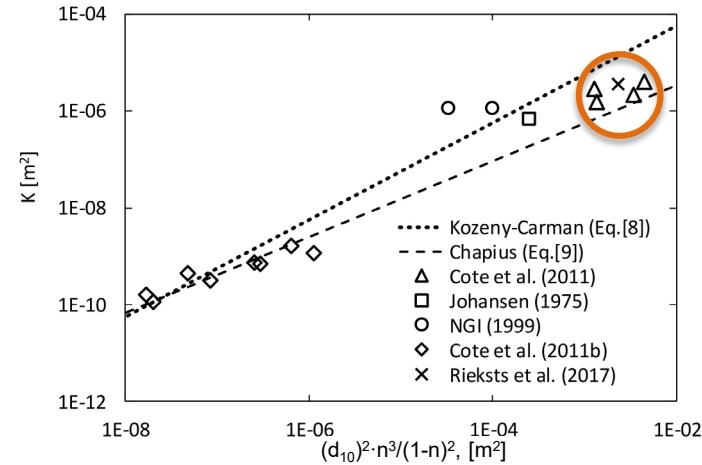
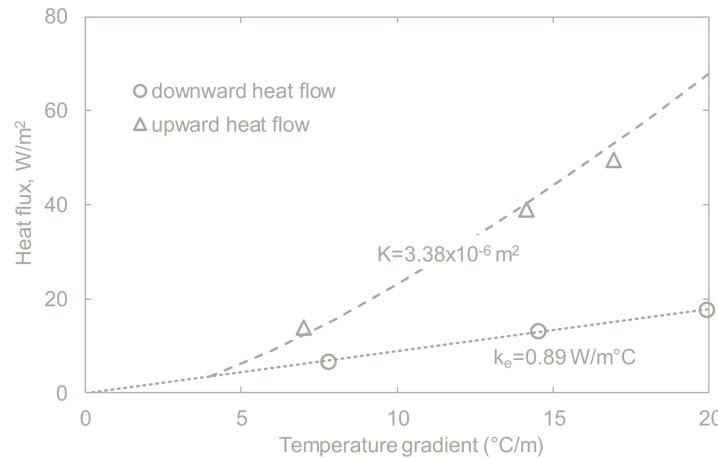


Upward heat flow:

$$\mathbf{q} = \nabla T$$

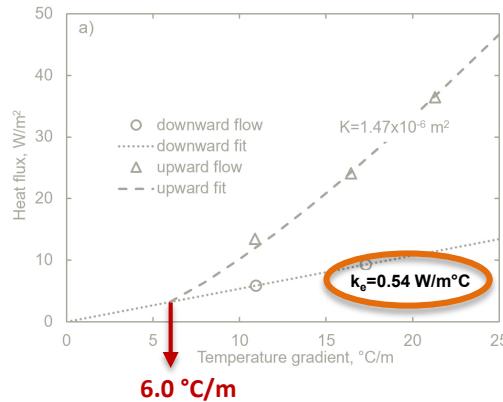


Validation for convective heat transfer with cobbles

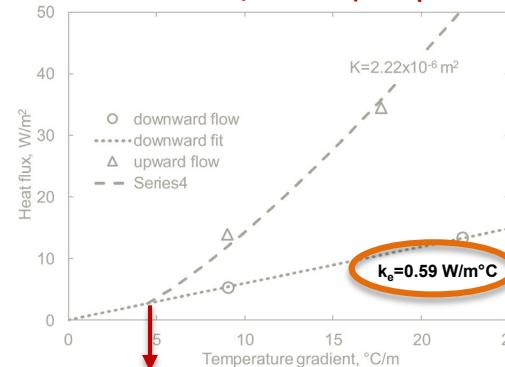


Convection in road construction materials

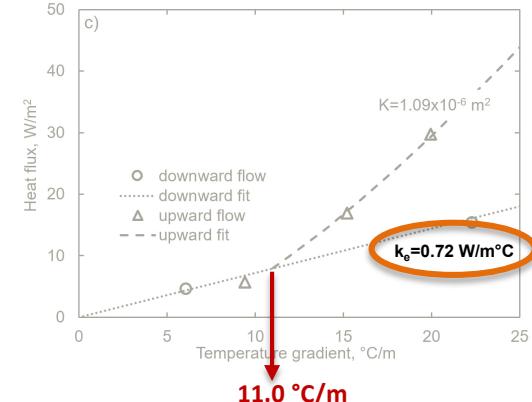
Crushed rock 20/120 mm (subbase)



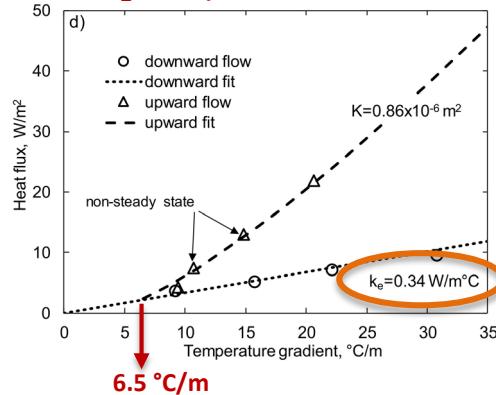
Crushed rock 40/120 mm (frost protection)



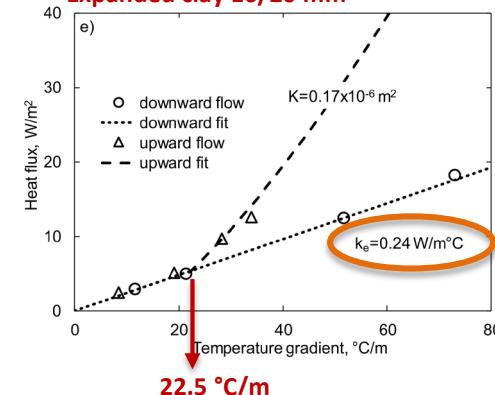
Crushed rock 20/250 mm (subballast)



Foam glass 10/60 mm



Expanded clay 10/20 mm



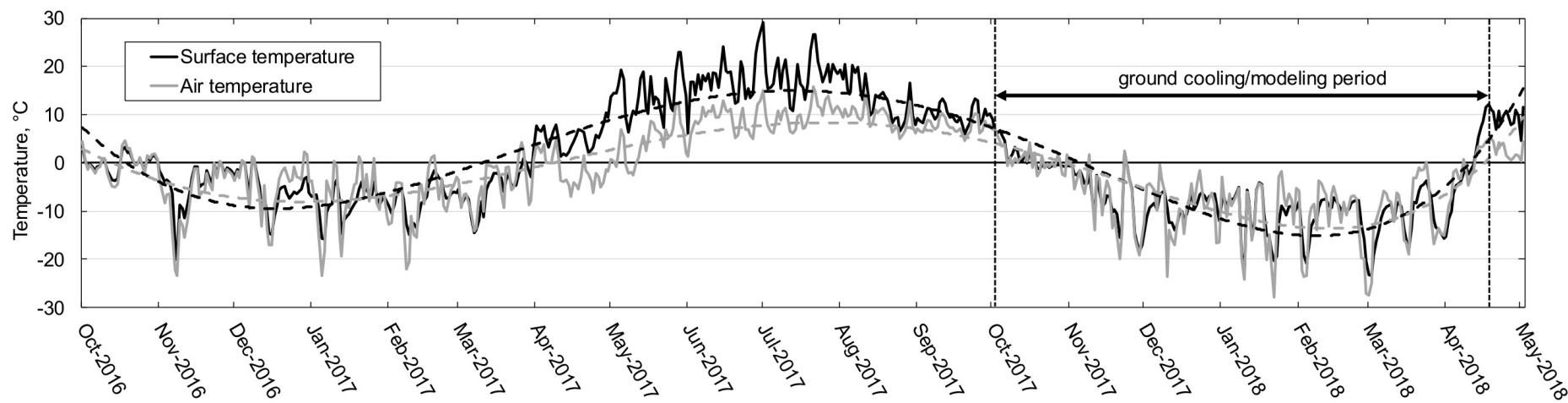
Constructed during fall of 2016

Road sections



Railway sections



**Winter 2016 / 2017**

$$FI_a = 25368 \text{ } ^\circ\text{C} \cdot \text{h} \quad (1057 \text{ } ^\circ\text{C} \cdot \text{days})$$

$$FI_s = 23160 \text{ } ^\circ\text{C} \cdot \text{h} \quad (965 \text{ } ^\circ\text{C} \cdot \text{days})$$

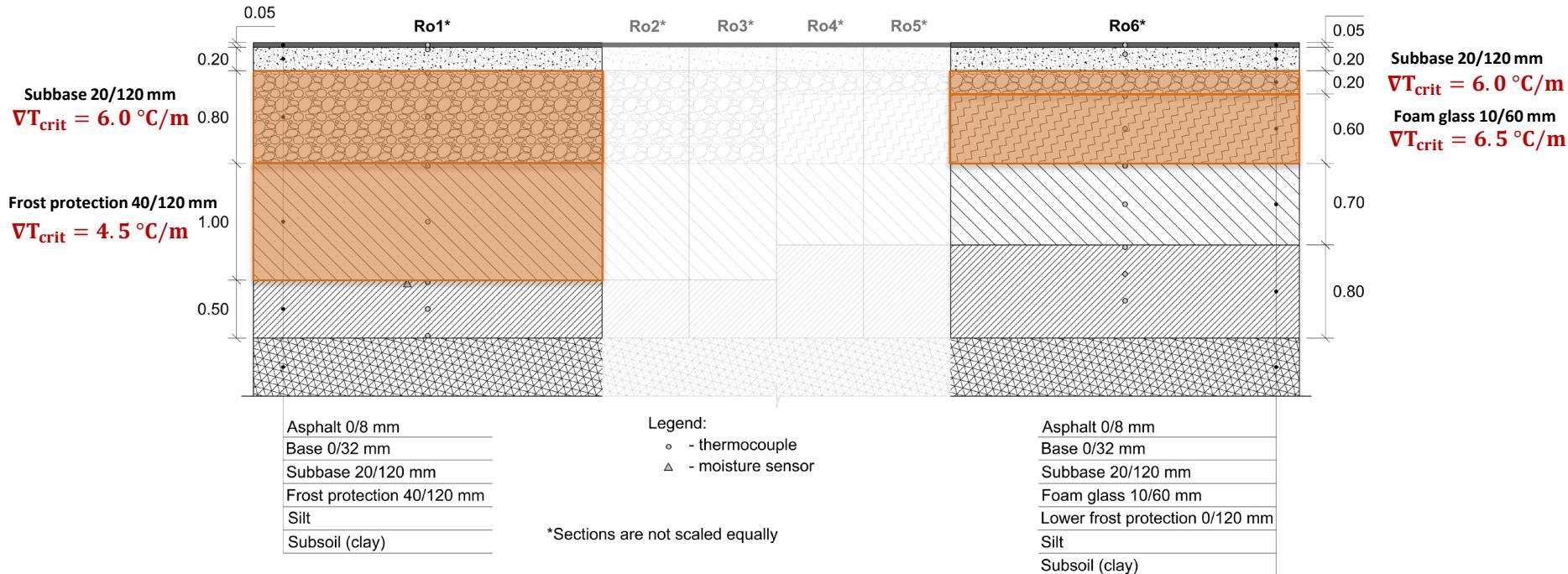
Winter 2017 / 2018

$$FI_a = 36864 \text{ } ^\circ\text{C} \cdot \text{h} \quad (1536 \text{ } ^\circ\text{C} \cdot \text{days})$$

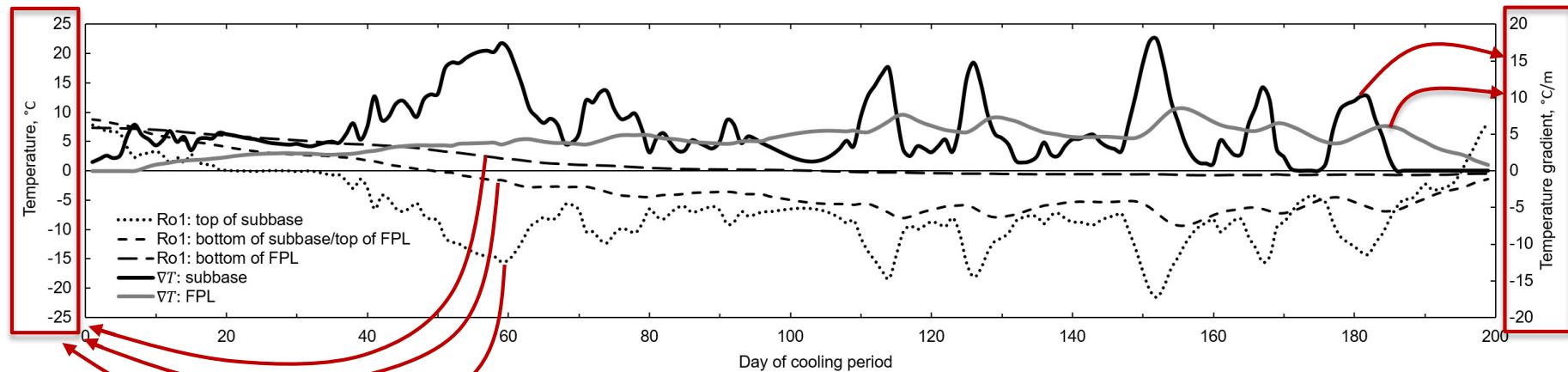
$$FI_s = 36744 \text{ } ^\circ\text{C} \cdot \text{h} \quad (1531 \text{ } ^\circ\text{C} \cdot \text{days})$$

Period of analysis: October 2, 2017 to April 19, 2018 → 200 days

Convection in road structural layers



Road section Ro1



Subbase 20/120 mm

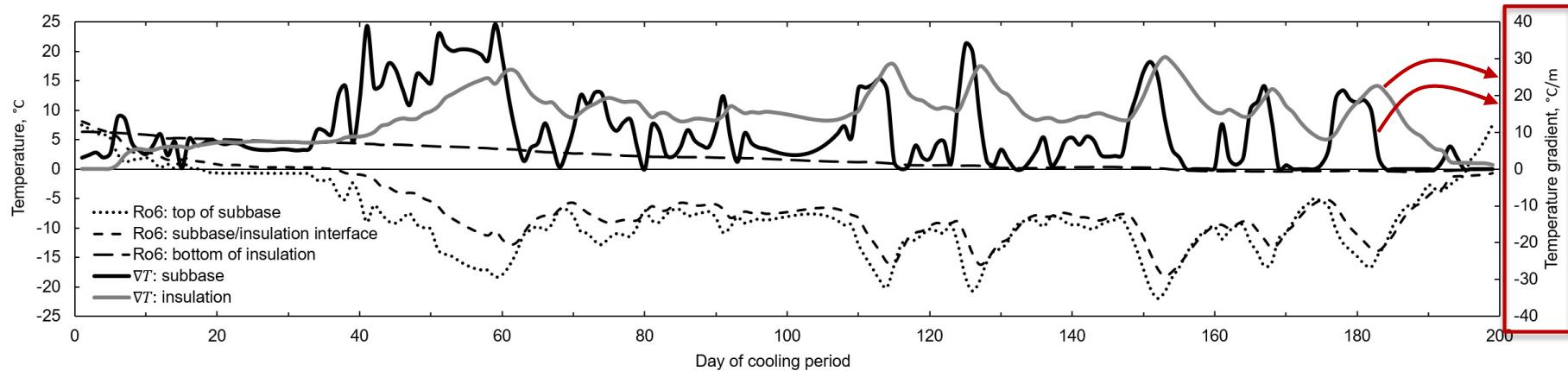
$$\nabla T_{\text{crit}} = 6.0 \text{ °C/m}$$

35% of time higher than 6.0 °C/m

Frost protection 40/120 mm

$$\nabla T_{\text{crit}} = 4.5 \text{ °C/m}$$

32% of time higher than 4.5 °C/m

Road section Ro6**Subbase 20/120 mm**

$$\nabla T_{\text{crit}} = 6.0 \text{ °C/m}$$

49% of time higher than 6.0 °C/m

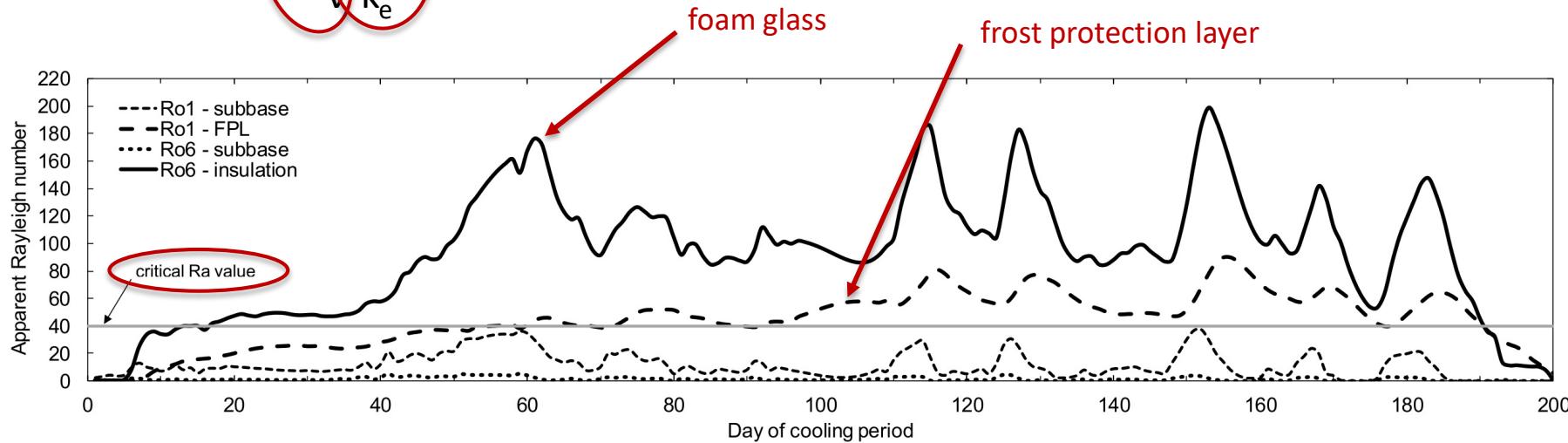
Foam glass 40/120 mm

$$\nabla T_{\text{crit}} = 6.5 \text{ °C/m}$$

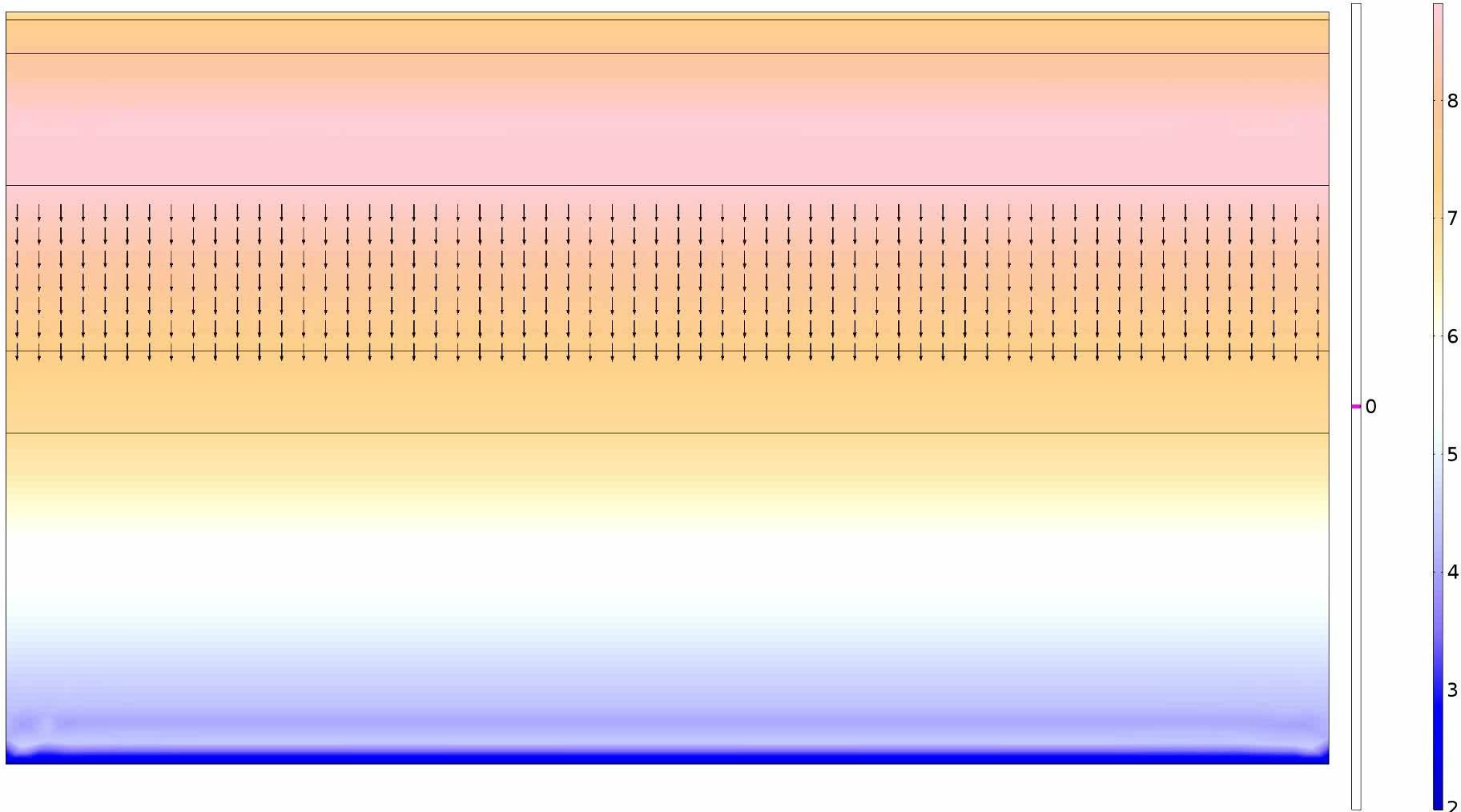
88% of time higher than 6.5 °C/m

$$Ra^* = \frac{g \beta C K H^2 \nabla T}{\nu k_e}$$

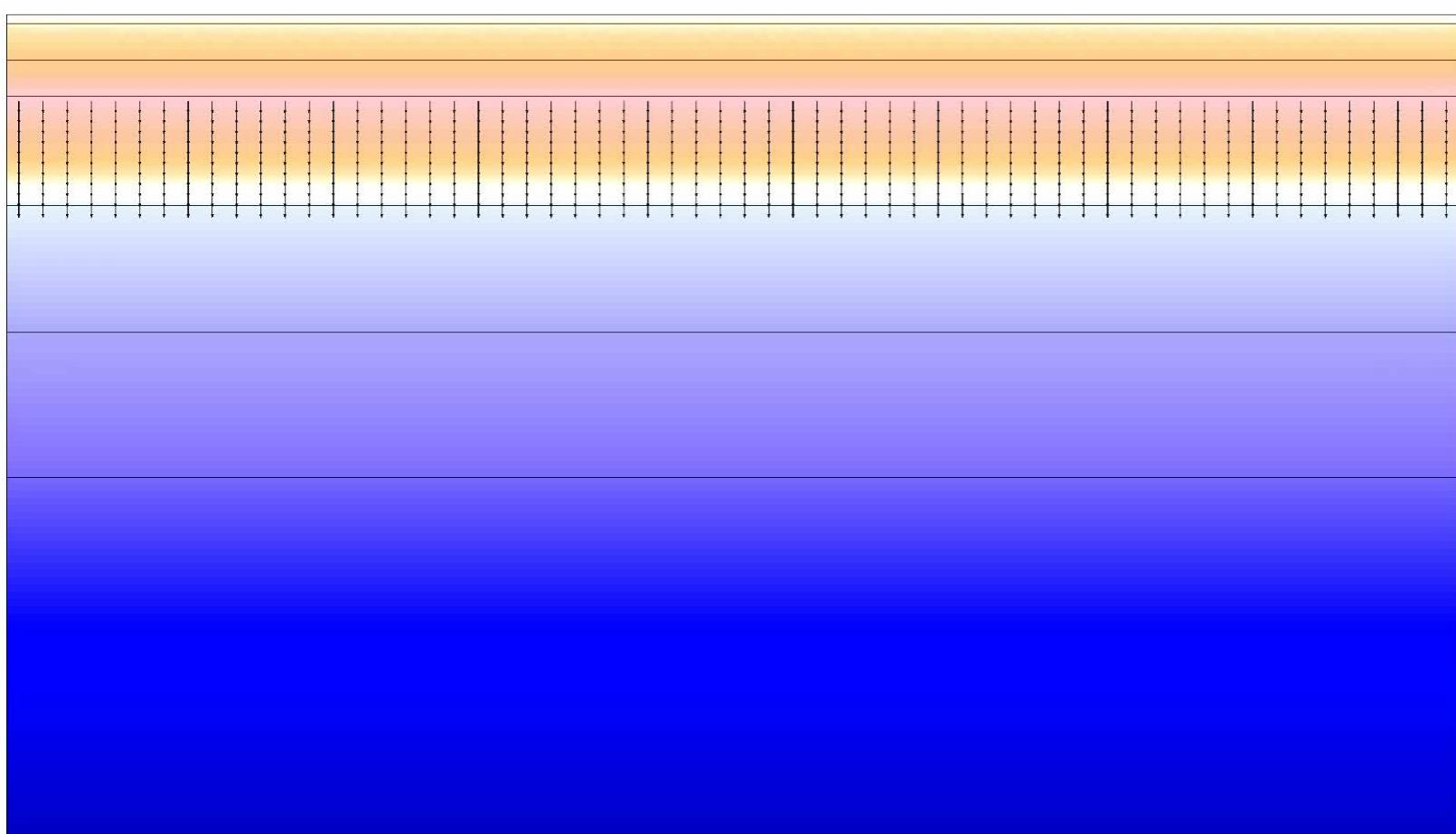
kept constant
adjusted depending on layer
variable



Road section Ro1

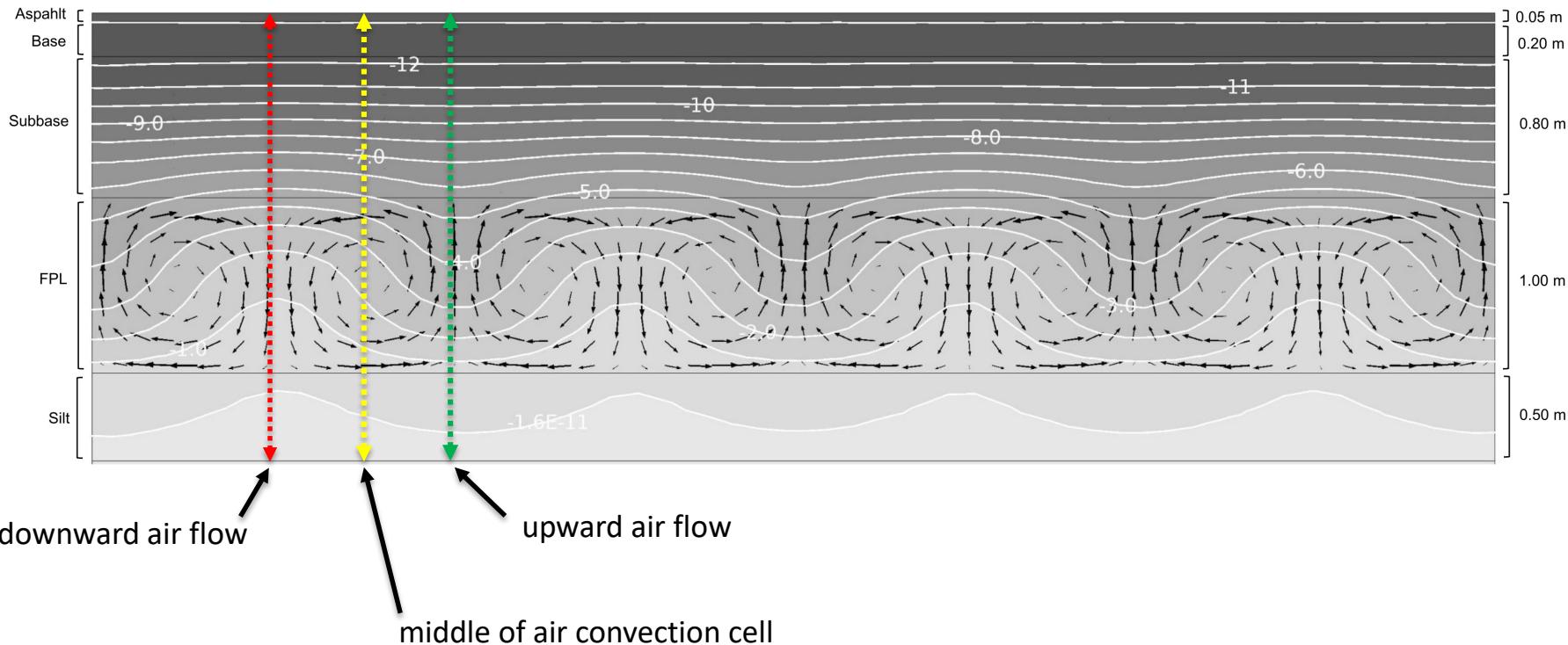


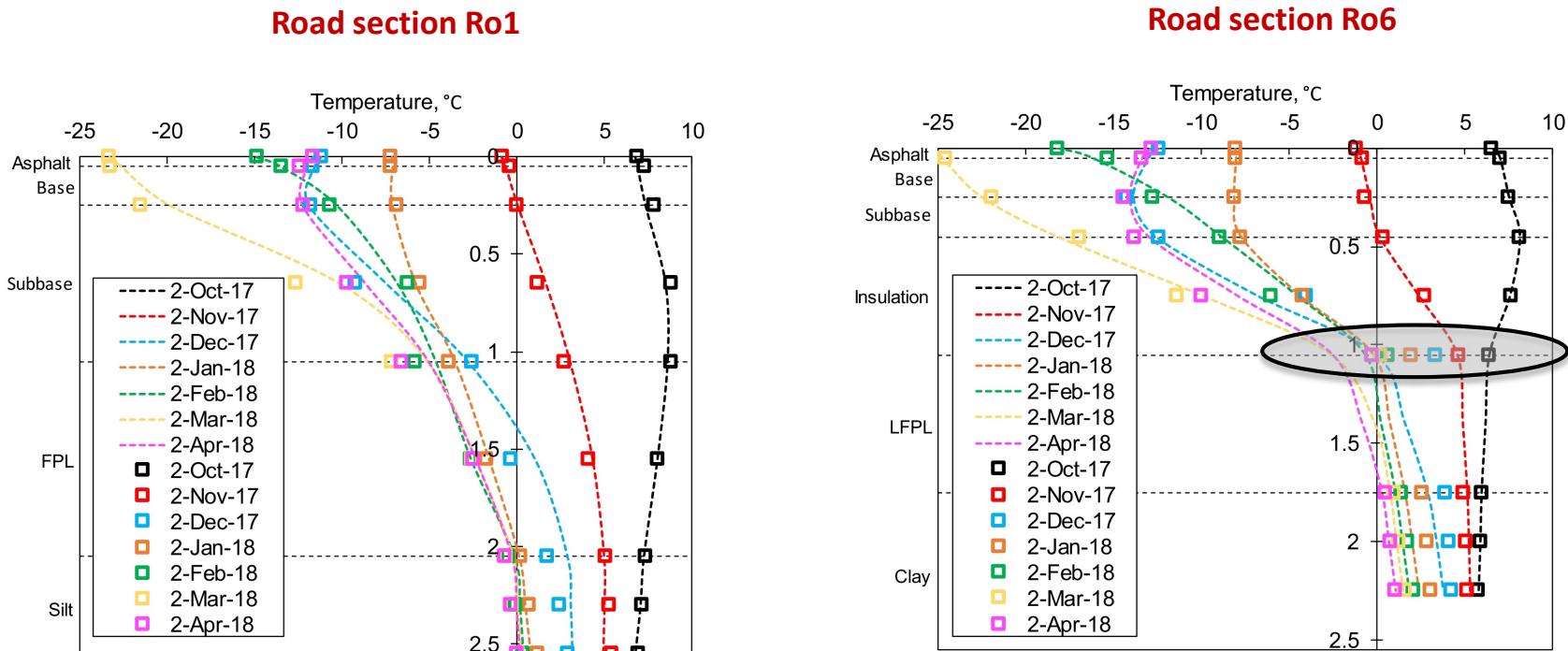
Road section Ro6



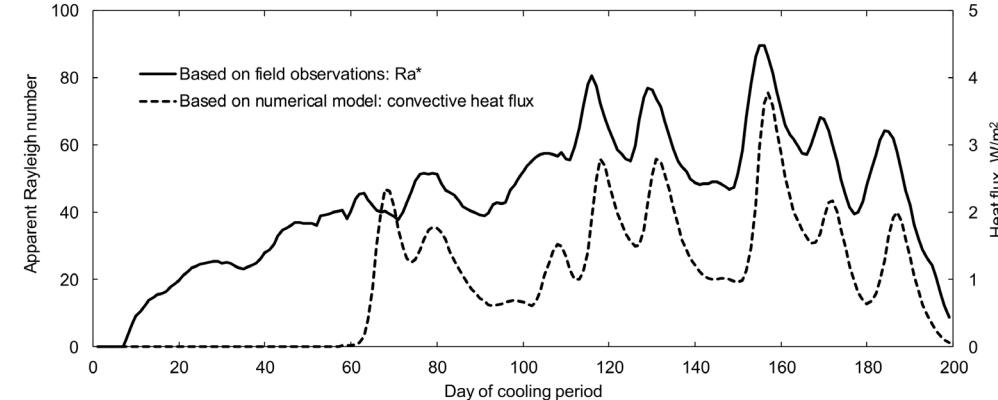
8
7.5
7
6.5
6
5.5
5

Road section Ro1



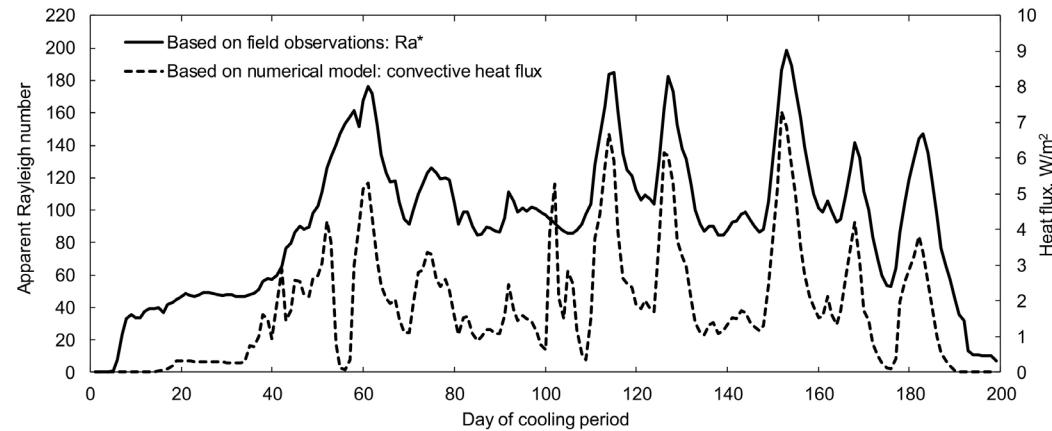


Road section Ro1



Convection in frost protection layer

Road section Ro6

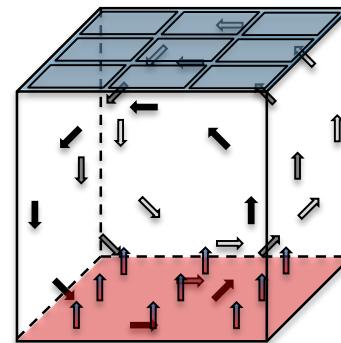
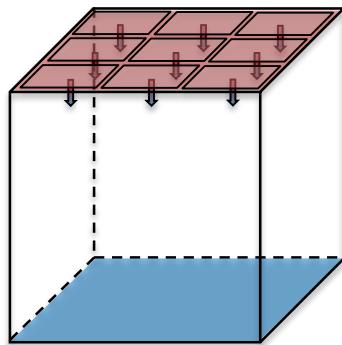


Convection in foam glass layer

Conclusion:

- Measurements of coarse-materials;
- Modelling;
- Frost protection layer – crushed rock materials;
- Coarse-subbase;
- Lightweight aggregates.

Thank you!



Norwegian University
of
Science and Technology



The Research Council
of Norway



Statens vegvesen
Norwegian Public Roads
Administration

